



Mechanics of deformable bodies
COE – 3001
Stress concentration
Homework #7

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Modeling assumptions

Unless otherwise stated, the following assumptions of strength of materials are adopted throughout this assignment:

- material is continuous, homogeneous, and isotropic,
- deformations are small,
- linear elastic behavior,
- stresses and strains are uniformly distributed,
- loads and supports are perfectly idealized.

Exercise I Power transmission through a stepped shaft

A stepped shaft rotates at $n = 900$ r/min. The allowable shear stress is $\tau_{\max} = 55$ MPa. The shaft geometry is characterised by a shoulder fillet of radius r .

Assume:

- The shaft is subjected to pure torsion.
- The stress concentration factor K_t is read from the standard abacus for a stepped shaft in torsion (see Figure 1).
- The material behaves as homogeneous, isotropic, and linearly elastic.

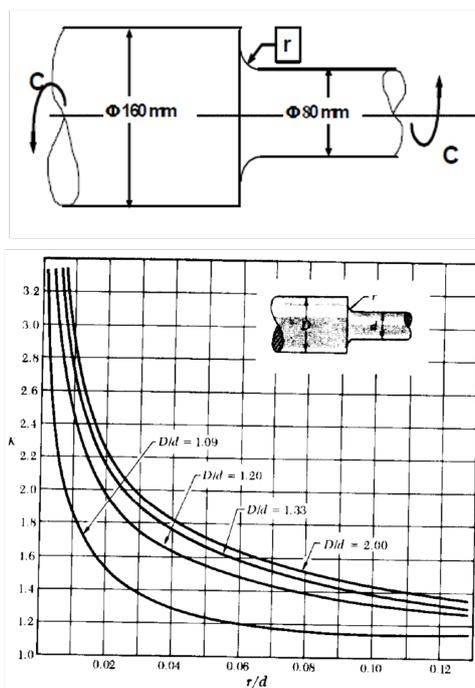


Figure 1: Stress concentration coefficient.

1. For a fillet radius $r = 4$ mm, read the stress concentration factor K_t from the abacus. Deduce the allowable nominal shear stress τ_{nom} , then compute the maximum torque T the shaft can transmit. Conclude by calculating the transmitted power P in kW.
2. For a fillet radius $r = 10$ mm, repeat the procedure. Compute the new transmitted power P' and determine the gain or loss in power with respect to question 1. Comment on the effect of the fillet radius on the load-carrying capacity.

Exercise II Stress concentration around a circular hole – Kirsch solution

An infinite thin plate of thickness $t = 5$ mm contains a small circular hole of radius $a = 4$ mm. The plate is subjected to a remote uniaxial tensile stress $\sigma_\infty = 80$ MPa applied along the x -axis. The material is linearly elastic with yield strength $\sigma_y = 250$ MPa.

The Kirsch solution gives the hoop stress $\sigma_{\theta\theta}$ at the hole boundary ($r = a$):

$$\sigma_{\theta\theta}(a, \theta) = \sigma_\infty (1 - 2 \cos 2\theta) \quad (1)$$

Assume:

- Plane stress conditions apply.
 - The plate is infinite: edge effects are neglected.
 - Small strains and linear elasticity hold throughout.
1. Determine the positions θ at which $\sigma_{\theta\theta}$ is maximum and minimum. Compute the corresponding stress values and deduce the theoretical stress concentration factor K_t .
 2. At $\theta = 90^\circ$, compute the maximum stress and check whether the material remains elastic. Define the load σ_∞^* at which first yielding occurs at the hole boundary.
 3. The plate is now subjected to equibiaxial tension: $\sigma_x^\infty = \sigma_y^\infty = \sigma_\infty$. Using the Kirsch solution for this loading state:

$$\sigma_{\theta\theta}(a, \theta) = 2\sigma_\infty \quad (2)$$

compute K_t and compare with the uniaxial case. Interpret physically the absence of θ -dependence.

4. The remote stress is now pure shear: $\tau_{xy}^\infty = \tau_0 = 40$ MPa, giving:

$$\sigma_{\theta\theta}(a, \theta) = -4\tau_0 \cos 2\theta \quad (3)$$

Determine the maximum hoop stress, the corresponding K_t (defined with respect to τ_0), and the angle θ at which it occurs.